



Optimization of the casting process from environmentally friendly bentonite-based sand for efficient casting during melting in an electric arc furnace

K.U. Tashxodjajeva^{1,2}

¹Tashkent State Technical University, University str., 2, Tashkent, Uzbekistan;

²Uzbek-Japan innovation center of youth, Laboratory of mechanical engineering and materials science, Tashkent, Uzbekistan

N.D. Turakhodjajev^{1,2}

¹Tashkent State Technical University, University str., 2, Tashkent, Uzbekistan;

²Uzbek-Japan innovation center of youth, Laboratory of mechanical engineering and materials science, Tashkent, Uzbekistan

SH.N. Turakhudjaeva³

³Turin Polytechnic University in Tashkent, Tashkent, Uzbekistan; Email: anvarovichsarvar908@gmail.com

ABSTRACT

Foundry production is one of the most diverse industries. In the foundry, several methods are used to manufacture a part. It includes processes such as centrifugal casting, permanent casting, die casting and sand casting. The article presents the process of casting into sand molds with bentonite. In the article, the authors conducted comparative studies of the reduction of marriages by porosity. In the course of the experiments, relevant analyses and conclusions are presented.

Keywords:

sandy shape, bentonite, porosity.

Introduction

Sand casting is one of the widespread technologies that uses sand as a refractory medium to increase the quality of casting. The entire production cycle of casting can be reduced to: model creation, forming and manufacturing of the rod, melting and casting, forging, testing and control. Most defects occur during the casting process. One of the sources of castings rejection is a shrinkage defect. Shrinkage is taken into account when casting cast iron and steel. It should be noted that the use of profits is justified when casting metals with a small solidification interval, because, otherwise, the metal in the main part and the profit will solidify simultaneously and the gases

will not have time to gather in the place reserved for them. The metal shrinkage defect significantly affects the casting efficiency. Also, one of the problems of foundry production is a porosity defect [1-2].

The molding mixture from which the mold is obtained must have a number of properties, the most important of which is strength, gas permeability, plasticity, compactness, etc. These properties of the mixture depend both on the quality and quantity of the initial components (quartz sand, waste mixture, bentonite or clay, binding additives, water, etc.) so it depends on the method of preparation of the mixture [3-5].

A two-stage process in which quartz is wetted with a binder (non-standard and

stationary state) is important for the practice of forming sand with the addition of a diluent to hang the strength in the solidified state. Sand-clay liners use expanding clay as a filler to fill sand voids and thus reduce the hydraulic conductivity of the mixture. The use of bentonite can lead to significant volume changes as a result of swelling and shrinkage. To improve compressibility and swelling, it is proposed to add a portion of clay with less plasticity than bentonite. It was found that adding less plastic soil material to bentonite

reduces its amount by 60-70% for a clay content of 10-50%, respectively. It was also found that the swelling pressure and the percentage of swelling were significantly reduced [6-8].

Materials

Sand casting is one of the most commonly used metal casting processes due to its inherent advantages in production, low cost and high productivity.

The prepared molding mixture is shown in Table 1.

Table 1. The prepared molding mixture

Used sand, %	Quartz sand, %	Bentonite, %	Water, %	Flamethrower chalk, mm	Drying form °C	Keeping the form dry, s
61-66	20-22	6-7	4-5	1-2 mm	100	4-6

Research and methods

The prepared casting model (Fig.1) is installed in the center of the flask with a rod (table 2), and a laboratory-tested molding mixture (Fig.2,3,4). The mold of the flask is filled and compacted, then the second half of the flask is installed on the model and filled with a molding mixture. The mixture is compacted, then fixing pins, filling necks and ventilation ducts are mounted. Profits are set at the same time, the profit walls are made conical with a decrease in the direction of the model. Such

profit generation is necessary to reduce melt shrinkage and remove gas bubbles.

The two halves of the flask are separated and the model is removed, and the mold is sent to dry for 4-6 hours at 100 °C [9-11]. The finished mold is filled with molten metal through the filler neck – casting and profit. After cooling the melt, the mold is destroyed, the part is cleaned of sand, excess metal in the form of a gate, profits, then sent for heat treatment and machining [12].

Table 2.

Quartz sand, %	Sulfite-alcohol bard, %	Bentonite, %
80 - 85	8 - 10	3 - 5



Fig.1. Casting model.



Fig.2. Test samples.



Fig.2. Strength, MA-500. kg/cm².



Fig.4. Moisture meter MA 150 Sartorius.

Results

Table 3. Laboratory data results.

Nº	Indicators	Sample1	Sample2	Sample3	Sample4	Sample5
1	Strength kg/cm ²	0,57	0,55	0,60	0,58	0,57
2	Humidity %	5,3	4,7	5,2	6,7	6,1
3	Gas permeability %	119	121	126	123	119



Fig.5. Top view of the form.



Fig.6. Bottom view of the form.

Conclusions

Based on the results obtained, the following conclusion can be drawn:

1. The configuration of the profits made by the cone-shaped allows the molten metal to be distributed more evenly over the entire height, while improving

the removal of gas from it with a test tube.

2. Replacing kaolin with bentonite saves energy resources three times.
3. The addition of gil bentonite reduced swelling and thereby preserved the structural dimensions of the part.

References

1. Muawia A. Dafalla The Compressibility and Swell of Mixtures for Sand-Clay Liners. *Advances in Materials Science and Engineering*. Volume 2017, Article ID 3181794, 9 pages.
2. M. A. Dafalla and A.M. Al-Mahbashi, "Effect of adding natural clay on the water retention curve of sand—bentonite mixtures," in *Unsaturated Soils: Research & Applications*, pp. 1017–1022, CRC Press, 2014.
3. А.Джосон. Технологии литья и формования металлических деталей. Путеводитель, Политехническое издательство, Тимишоара, 2012 г.
4. Tursunbaev, S., Umarova, D., Kuchkorova, M., & Baydullaev, A. (2022, June). Study of machining accuracy in ultrasonic elliptical vibration cutting of alloyed iron alloy carbon with a germanium. In *Journal of Physics: Conference Series* (Vol. 2176, No. 1, p. 012053). IOP Publishing.
5. Ana Josen, Camelia Pinsa-Bretotean, Sorin Ratiu. Engineering and Manajment Department. University of Timisoara, Hunedoary, Romania.
6. Тураходжаев, Н. Д., Ташбулатов, Ш. Б., Турсунбаев, С. А., Турсунов, Т. Х., & Абдуллаев, Ф. К. (2020). Исследование анализа извлечения меди и алюминия из шлаков в дуговой печи постоянного тока. In *Техника и технологии машиностроения: материалы IX Междунар. науч.-техн. конф. (Омск, 8–10 июня 2020 г.)*.—Омск: Изд-во ОмГТУ (pp. 68-70).
7. Bektemirov A.D., Tashkhodjayeva K.U., Erkinjonov A.B. "Development of technology for obtaining high-quality cast products from carbon steel alloy" *Scientific and technical journal of "Mashinasozlik" ISSN 2181-1539. № 2. 2022*
8. Turakhodjaev N.D. "Quality improvement of the steel melting technology in an electric arc furnace" *ACADEMIA 2021.-Т. 11.-№ 7. – pp.48-54.*
9. Турсунбаев, С. А. (2019). Особенности обработки деталей из магнитотвердых материалов. *ТЕХНИКА И ТЕХНОЛОГИИ МАШИНОСТРОЕНИЯ*, 23-27.
10. Турсунбаев, С. А., Зокиров, Р. С., & Тураев, Х. У. (2017). Влияние обработки деталей из алюминиевого сплава с применением высокоскоростных токарных станков на срок службы резца. *ТЕХНИКА И ТЕХНОЛОГИИ МАШИНОСТРОЕНИЯ*, 159-163.
11. Turakhodjaev, N., Odilov, F., Tursunbaev, S., & Kuchkorova, M. (2021). Development of technology for increasing endurance when crushing the working parts of shredders (crushers) in conditions of increased friction. *Техника и технологии машиностроения*, 71-76.
12. Sun, H., & Zhang, J. (2014). Study on the macrosegregation behavior for the bloom continuous casting: Model development and validation. *Metallurgical and materials transactions B*, 45, 1133-1149.